

Ontario Ministry of Transportation

Highway 17 Planning & Class EA Study Noise Review GWP 5670-10-00

Prepared by:

AECOM

5600 Cancross Court, Suite A 905.501.0641 tel Mississauga, ON, Canada L5R 3E9 905.501.0181 fax www.aecom.com

Project Number:

60241599

Date:

July, 2014

Distribution List

# of Hard Copies	PDF Required	Association / Company Name		
2	X	Ministry of Transportation		

Revision Log

Revision #	Revised By	Date	Issue / Revision Description

AECOM Signatures

Report Prepared By:	
	James Au, P.Eng., INCE
	Acoustic Engineer
Report Prepared By:	
	Brian Bulnes, EIT
	Acoustic Engineering Intern
Report Reviewed By:	
	Alex Dundon, P.Eng., INCE, MIEAust
	Senior Acoustic Engineer

Executive Summary

The Ontario Ministry of Transportation has retained AECOM to undertake a Class Environmental Assessment to identify a recommended plan for a four-lane Highway 17 within the study limits with access restricted to interchange locations.

The planning alternatives included segments of widening/improving the existing highway and segments of realigned highway, with interchanges at key connection points and new service roads for some areas. In the Rutherglen and Amable du Fond areas, widening of the existing highway is not possible due to physical constraints and environmental conditions. Therefore, realignment alternatives were generated for these two areas while widening alternatives were generated for the Pimisi Bay and Pautois Creek areas. The evaluation of highway planning alternatives was completed on a comparative basis for each of the four highway realignment and widening alternative areas (with associated interchanges and service roads) and a recommended plan was identified in January 2014, prior to this assessment being conducted.

A detailed noise assessment was completed for the recommended plan which includes improvements to Highway 17 from an undivided two lane highway to a four lane controlled access divided freeway along a new alignment.

According to noise predictions, the proposed changes to Highway 17 would result in medium to high changes in noise level perception at several nearby receptors (e.g. residences) due to the realigned portions of the highway, which are primarily in greenfield areas. The noise assessment has been completed using predicted 2035 traffic volumes.

At one location (R18), a noise barrier appears to be warranted based on MTO policy. The necessity for noise mitigation, (as presented in Section 4.2), is recommended for further exploration and examination during detail design for one receptor (R18) where initial analysis indicates that:

- The increase in noise caused by the recommended plan at this location is greater than 5 dB;
- A noise barrier at this location with a height of 5 metres and a length of 28 metres would meet the minimum noise reduction requirement of 5 dB; and
- A noise barrier is considered economically feasible because the barrier cost per household is less than the MTO rule of thumb 'ballpark' cost limit of \$100,000 per receptor.

Noise resulting from construction of the recommended plan varies based upon a variety of factors such as time and location of operation, size and concurrent use of equipment, and staging of construction. As equipment information is only available from the contractor that is awarded the construction contract, general recommendations to minimize the impact of construction noise have been provided.

Table of Contents

Distribution List Executive Summary

			page
1.	Intr	oduction	1
2.	Env	rironmental Highway Traffic Noise Guidelines	3
	2.1	Criteria	3
	2.2	Noise Sensitive Areas	4
3.	Ass	essment of the Recommended Plan – Methodology	5
	3.1	Traffic Data	5
	3.2	Area of Investigation	5
	3.3	Areas Requiring Detailed Assessment	
	3.4	Noise Prediction Procedure	7
4.	Ass	essment of the Recommended Plan – Results and Recommendations	9
	4.1	Results	9
	4.2	Noise Mitigation Investigation	9
5.	Con	nstruction Noise	12
	5.1	Municipal Noise Control By-Laws	12
	5.2	Construction Noise Control Recommendations	12
6.	Con	nclusions/Recommendations	15
7.	Ref	erences	16
List	of Fig	jures	
Figur	e 1.1:	Class EA Study Limits	1
List	of Tal	bles	
Table	2.1:	MTO Criteria for Investigation of Noise Mitigation	3
Table	2.2:	Perceived Impact of Increased Sound Levels	4
Table	3.1:	Traffic Data	5
		Assessed Noise Sensitive Locations	
Table	4.1: N	oise Assessment Results – Most Exposed Side	9
Table	e 4.2:	Predicted Noise Reduction by Noise Barrier	10
Table	4.3:	Resultant Noise Barriers and Approximate Costing	10

Appendices

Appendix A: Recommended Plan Appendix B: Area of Investigation

Appendix C: Detailed Assessment Receptor Locations

Appendix D: Zoning Plan

Appendix E: Proposed Noise Barriers

Appendix F: Traffic Data

Appendix G: Traffic Noise Calculations

1. Introduction

The Ontario Ministry of Transportation has retained AECOM to undertake a Class Environmental Assessment to identify a recommended plan for a four-lane Highway 17 within the study limits with access restricted to interchange locations. The study limits are shown in **Figure 1.1** below and involve a 23.5 km section of Highway 17 from Bonfield easterly to the boundary road between the Townships of Calvin and Papineau-Cameron.

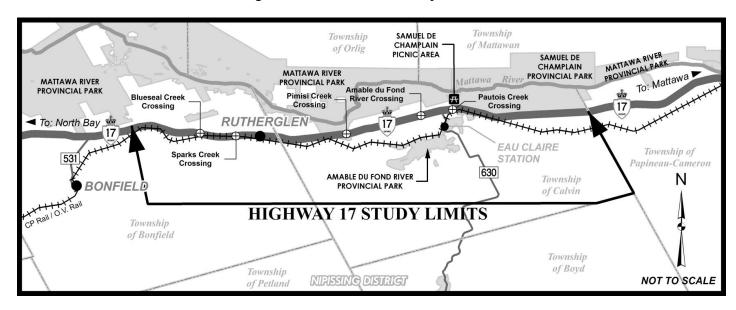


Figure 1.1: Class EA Study Limits

Within the Study Area, Highway 17 is primarily a two lane highway with limited access restrictions and access in both directions provided via private driveways and local roadways. This planning, preliminary design and Class EA study has been completed to identify a preferred plan for Highway 17 to improve future traffic operations and to enhance highway safety from Bonfield to the boundary road of Calvin Township and the Township of Papineau-Cameron.

As outlined in the Study Design Report (AECOM 2012) for this project, the study involved the development and evaluation of a range of alternatives which could address the transportation needs of the study area. Specifically, the alternatives considered included:

- widened/improved provincial highway;
- realigned provincial highway; and
- · combinations of the above.

The cross section for the highway is a freeway with two lanes in each direction and a 30m median within a total right-of-way width of 110m, and access restricted to interchanges. Highway planning alternatives were generated within the Study Area and in consideration of the environmental constraints. The planning alternatives included segments of widening/improving the existing highway and segments of realigned highway, with interchanges at key connection points and new service roads for some areas. In the Rutherglen and Amable du Fond areas, widening of the existing highway is not possible due to physical constraints and environmental conditions. Therefore, realignment alternatives were generated for these two areas while widening alternatives were generated for the Pimisi Bay and Pautois Creek areas. The evaluation of highway planning alternatives was completed on a comparative basis for

each of the four highway realignment and widening alternative areas (with associated interchanges and service roads) and a recommended plan was identified in January 2014 as shown in **Appendix A**.

The purpose of this report is to document the detailed noise assessment undertaken for the recommended plan to identify noise impacts and potential noise mitigation.

2. Environmental Highway Traffic Noise Guidelines

2.1 Criteria

This assessment has been completed in accordance with the requirements stipulated in MTO's *Environmental Guide for Noise* (the Guide) published in 2006.

Under the Guide, the "noise impact" is defined as the difference between the "No Project" and the "With Project" noise levels during the subject year of assessment (Horizon Year), which is typically 10 years post-construction.

The Guide requires that the most exposed side of a dwelling unit be assessed as part of an initial screening. If the initial screening indicates that noise mitigation investigation is required, the point of assessment for determining the noise mitigation requirements is the Outdoor Living Area (OLA).

The OLA can be situated on any side of a noise sensitive area which accommodates outdoor living activities, and is generally taken to be the backyard. For this assessment, the location has been taken as 3 metres from the façade with a height of 1.2 metres above ground level.

The criteria for investigating potential noise mitigation are based on both the noise impact and the overall noise level due to the project. These criteria are outlined in **Table 2.1**.

Table 2.1: MTO Criteria for Investigation of Noise Mitigation

Change in Noise Level Above Future Ambient ¹ /Projected Noise Levels with Proposed Improvements	Mitigation Effort Required
< 5 dB Change AND <65 dBA Overall	• None
≥ 5 dB Change OR ≥ 65 dBA Overall	 Investigate noise control measures on right of way Introduce noise control measures within right of way and mitigate to ambient if technically, economically, and administratively feasible. Noise control measures, where introduced, should achieve a minimum of 5 dBA attenuation, over first row receivers.

The Guide recognizes that an important assessment criterion for the existing dwellings is the change in noise level above ambient sound levels. **Table 2.2** complements the Guide by providing the perceived impact of changes in sound level.

¹ Noise impact

Table 2.2: Perceived Impact of Increased Sound Levels²

Increased Sound Level Above Ambient (dB)	Perception	Perceived Impact	
0 to 3	Potentially Perceptible	Minor	
3 to 5	Perceptible	Low	
5 to 10	Up to twice as loud	Medium	
Greater than 10	Twice as loud or greater	High	

2.2 Noise Sensitive Areas

Predicted noise levels are assessed at noise sensitive areas. Land uses designated as noise sensitive by the MTO *Environmental Guide for Noise* consist of the following:

- Private homes such as single family residences (the only applicable land use for this study)
- Townhouses
- Multiple unit buildings, such as apartment buildings with OLAs for use by all occupants
- Hospitals, nursing homes for the aged, where there are OLAs for the patients

Land uses that do not qualify as noise sensitive by the MTO Environmental Guide for Noise consist of the following:

- · Apartment balconies above ground floor
- Educational facilities (except dormitories with OLAs)
- Churches
- Cemeteries
- Parks and picnic areas which are not inherently part of a NSA
- Daycare centres
- All commercial and industrial areas

² Adapted from "Engineering Noise Control, Theory and Practice" 4th edition, David A. Bies and Colin H. Hansen, 2009

3. Assessment of the Recommended Plan – Methodology

Several options, including the Do Nothing option, were considered early in the Environmental Assessment process and were eliminated from further consideration as these options did not address the long term operational safety and capacity goals (2035 subject year of assessment) for the highway and therefore did not address the objectives of the project. The assessment of the recommended plan was based on the predicted overall noise level and the noise impact, which is defined as the noise level difference between:

- No Project no changes to the existing road configuration.
- With Project a four lane divided controlled access freeway along a widened / realigned alignment, replacing the existing Highway 17. The recommended plan for the highway is shown in **Appendix A**.

3.1 Traffic Data

The road traffic data is summarized in **Table 3.1.1**. The road improvements for this project are planned to improve the safety along the highway within the study limits and increase the long term traffic capacity. The total traffic volume for both the No Project and With Project options are the same. Given that the With Project option sees the highway divided and a wide median implemented, the total traffic volume was equally divided to reflect the two directions of travel on the widened/realigned highway. The traffic volumes were not divided for the No Project option as the lanes of travel are immediately adjacent to one another. All road traffic data referenced below is provided in **Appendix F**.

	No Project (2035)			New Alignment (2035)			General Characteristics				
Source	SADT	%M.T.	%Н.Т.	Speed Limit (kph)	SADT	%M.T.	%Н.Т.	Speed Limit (kph)	Grade %	Pavement Type	Day/Night Split
Existing Highway Alignment	10200	5.77	9.23	90	-	-	-	-	<2	1	85/15
New Highway Alignment EB	-	-	-	-	5100	5.77	9.23	100	<2	1	66/33
New Highway Alignment WB	-	-	-	-	5100	5.77	9.23	100	<2	1	66/33

Table 3.1: Traffic Data³

3.2 Area of Investigation

The area of investigation was determined by creating 5 dB contour lines from the proposed project to where there is no predicted increase over the future ambient noise levels. The approved prediction methodology in the Guide (Ontario Road Noise Analysis Method for Environment and Transportation – ORNAMENT) is a receptor based prediction methodology, using text inputs and outputs to create a separate model for each receptor. This does not lend itself to creating noise contours.

To generate noise contours, a graphical noise prediction software (CADNA/A), implementing a different prediction methodology (ISO 9613-2), was calibrated to approximate ORNAMENT results. A variation of only +/- 1dB is expected over typical gentle sloping terrain. Topography was not incorporated into the generation of the noise contours as the prediction models differ too greatly in terms of topography effects on noise prediction; because the

³ SADT – Summer Average Daily Traffic

[%]M.T. – Medium Truck Percentage

[%]H.T. - Heavy Truck Percentage

purpose of the noise contours is to identify the areas requiring detailed assessment, where established criteria is potentially met and/or exceeded.

The noise contours are presented in Appendix B, with the areas requiring a detailed assessment using the approved STAMSON prediction methodology presented in Section 3.3.

The Study Area can be classified as a Class 3 rural area as per the definitions provided in various Ministry of the Environment Ontario (MOE) noise guidelines. Where no dominant sources of noise exist, the Guide suggests an ambient noise level of 45 dBA for Class 3 areas. Therefore, the future No Project ambient noise levels in the Study Area were taken as the greater of 45 dBA or the future No Project noise levels due to the existing roadways.

3.3 Areas Requiring Detailed Assessment

A review of the Study Area and the noise contours prepared as described in the above section indicates that there are several noise sensitive areas north and south of the alignment that require a detailed noise assessment. The noise sensitive areas consist of several single residences and a group of three residences in one area.

Eighteen assessment locations have been identified as representative of the worst case noise sensitive locations. These locations are detailed in **Table 3.2** and on the plan provided in **Appendix C**, with zoning plans provided in **Appendix D**.

Table 3.2: Assessed Noise Sensitive Locations

Assessment Location	Description	Receptors Represented
R01	South of Highway 17, 1.02km from Highway 17 and Trout Pond road intersection.	Group of three residences
R02	South of Highway 17, 414 metres east along Trunk road from Trunk and Fichault road intersection, and 146 metres north of trunk road.	Single residence
R03	South of Highway 17, 597 metres east along Trunk road from Trunk and Fichault road intersection, and 24 metres south of Trunk road.	Single residence
R04	South of Highway 17, 818 metres right from Trunk and Fichault road intersection, and 98 metres north of Trunk road.	Single residence
R05	South of Highway 17, 939 metres east along Trunk road from Trunk and Fichault road intersection, and 142 metres south of Trunk road.	Single residence
R06	South of Highway 17, 384 metres west along Trunk road from Trunk and McNutt road intersection, and 45 metres north of trunk road.	Single residence
R07	South of Highway 17, 286 metres west along Trunk road from Trunk and McNutt road intersection and 106 metres south of Trunk road.	Single residence
R08	South of Highway 17, 392 metres south along McNutt road from Trunk and McNutt road intersection and 220 metres west of McNutt road.	Single residence
R09	South of Highway 17, 750 metres along McNutt road southeast of Trunk and McNutt road intersection.	Single residence
R10	South of Highway 17, 1.02 km southeast along Rutherglen line from Trunk road and Rutherglen line intersection.	Single residence
R11	55 metres south of Highway 17, 767 metres west from Highway 17and Columbia road intersection along Highway 17.	Single Residence
R12	35 metres north of Highway 17, 407 metres east from Highway 17 and Columbia road intersection along Highway 17.	Single Residence

Assessment Location	Description	Receptors Represented
R13	100 metres north of Highway 17, 1.69 km west from the Highway 17 and Highway 630 intersection along Highway 17.	Single Residence
R14	493 metres south of Highway 17, along Highway 630, and 90 metres east from Highway 630.	Single Residence
R15	South of Highway 17, 118 metres along Suzanne road, east of the Suzanne and Donalds road intersection.	Single Residence
R16	322 metres south of Highway 17, 1.58 km west from the Highway 17 and Champlain Provincial Park road intersection along Highway 17.	Single Residence
R17	300 metres south of Highway 17, 1.32 km west from the Highway 17 and Champlain Provincial Park road intersection along highway 17.	Single Residence
R18	112 metres south of Highway 17, 548 metres east from the Highway 17 and Boundary road intersection along Highway 17.	Single Residence

3.4 Noise Prediction Procedure

As set out in the Guide, traffic noise levels were calculated using the Ontario Road Noise Analysis Method for Environment and Transportation (ORNAMENT) method, implemented in the STAMSON (version 5.04) software.

The prediction model inputs include the following considerations:

- Road traffic data (see Section 3.1)
 - Volumes
 - Speed limit
 - o Vehicle composition (percentage Medium and Heavy Trucks)
- Ground characteristics
 - o Roadway surface type (e.g. Asphalt, concrete)
 - Ground topography
 - Ground type between assessment locations and roadways
 - o Roadway layout
- Shielding effects
 - o Berms
 - Barriers
 - Housing

The traffic data used in the assessment of the recommended plan is described in Section 3.1.

As this project involves the widening and realignment of existing Highway 17 to a freeway cross section, the assessment of the noise levels was based on the 24 hour equivalent sound level ($L_{eq, 24hr}$) as required by the Guide. To assess the noise impact, the predicted "No Project" noise levels (year 2035) were compared to those of the predicted "With Project" noise levels (year 2035).

As required in the Guide, noise levels on the most exposed side of a noise sensitive land use were calculated to determine if a noise mitigation investigation would be required. If a noise investigation was required, the noise levels were assessed at the OLA location, which is the point of assessment for noise mitigation as noted in the Guide.

The modeling assumed a typical asphalt road surface would be used. If a concrete road surface is used, the With Project noise levels are expected to be up to approximately 3 dB higher than those levels detailed below.

Assessment of the Recommended Plan – Results and Recommendations

4.1 Results

Table 4.1 shows the predicted future "No Project" and "With Project" noise levels, as well as the resulting change in noise levels due to the recommended plan. Also shown in **Table 4.1** is the perception of the noise impact and the requirement for noise mitigation investigation. Calculation inputs are provided in **Appendix G**.

As indicated in **Section 3.2**, the Study Area can be classified as a Class 3 rural area as per the definitions provided in various Ministry of the Environment Ontario (MOE) noise guidelines. Where no dominant sources of noise exist, the Guide suggests an ambient noise level of 45 dBA for Class 3 areas. Therefore, the future No Project ambient noise levels in the Study Area were taken as the greater of 45 dBA or the future No Project noise levels due to the existing roadways.

Location		Projected Future Overall Traffic Noise $L_{\text{eq,24hr}}$ (dBA)		re Noise Impact	Mitigation Investigation Requirement		
	No Project	With Project	Change (dB)	Perception	≥65 dBA	≥5 dB impact	
R01	45.0	48.1	3.1	Low	No	No	
R02	45.0	50.9	5.9	Medium	No	Yes	
R03	45.0	52.0	7	Medium	No	Yes	
R04	45.0	58.6	13.6	High	No	Yes	
R05	45.0	50.9	5.9	Medium	No	Yes	
R06	50.3	52.5	2.2	Minor	No	No	
R07	45.0	50.3	5.3	Medium	No	Yes	
R08	45.0	58.3	13.3	High	No	Yes	
R09	45.0	51.1	6.1	Medium	No	Yes	
R10	45.0	55.7	10.7	High	No	Yes	
R11	59.1	66.7	7.6	Medium	Yes	Yes	
R12	64.3	57.3	-	-	No	No	
R13	56.7	53.3	-	-	No	No	
R14	48.1	61.0	12.9	High	No	Yes	
R15	45.0	50.4	5.4	Medium	No	Yes	
R16	48.7	56.5	7.8	Medium	No	Yes	
R17	49.6	57.6	8.0	Medium	No	Yes	
R18	56.4	61.9	5.5	Medium	No	Yes	

Table 4.1: Noise Assessment Results - Most Exposed Side

The noise level limit of 65 dBA is exceeded at one of the assessed locations (R11) and the noise impact exceeds the 5 dB criterion at the majority of the assessed areas (R02 through R05, R07 through R11 and R14 through R18). Noise mitigation investigation was therefore required for the OLAs of 14 assessed locations. The mitigation investigation is described in the following section.

4.2 Noise Mitigation Investigation

As required by the Guide, the OLA is the point of assessment for noise mitigation investigation; in the case of this project the OLAs are located on the most exposed side of the assessed locations.

Further investigation has been conducted to determine the feasibility of mitigating noise from the project. As per the Guide, noise mitigation must provide an average of at least 5 dB of attenuation over the first row of receptors. It is MTO's position, based upon their experience, that noise barriers with heights greater than 5 metres are considered impractical from cost and constructability standpoints. A summary of noise barrier performance is provided in **Table 4.2**.

Table 4.2: Predicted Noise Reduction by Noise Barrier

Assessment Locations (see Table 4.1 for Investigation	Projected Future Ov L _{eq,24hr} (Noise Reduction (dB)	Achieves 5 dB Reduction	
Requirement)	Unmitigated	Mitigated	,		
R02	50.9	45.2	5.7	Yes	
R03	52.0	47.2	4.8	No	
R04	58.6	53.3	5.3	Yes	
R05	50.9	45.6	5.3	Yes	
R07	50.3	49.6	0.7	No	
R08	58.3	54.6	3.7	No	
R09	51.1	51.1	0.0	No	
R10	55.7	50.7	5.0	Yes	
R11	66.7	66.7	0.0	No	
R14	61.0	60.4	0.6	No	
R15	50.4	50.4	0.0	No	
R16	56.5	56.5	0.0	No	
R17	57.6	57.6	0.0	No	
R18	61.9	56.9	5.0	Yes	

The above results indicate that a noise barrier with a height of 5 metres would meet the minimum noise reduction requirement of 5 dB for receivers R02, R04, R05, R10, and R18. Noise barriers providing the minimum 5 dB reduction requirement were consolidated to produce recommendations and approximate costing. This is summarized in **Table 4.3**.

Table 4.3: Resultant Noise Barriers and Approximate Costing

Assessment Locations	Receptors with 5 dB Reduction	Barrier Height (m)	Barrier Length (m)	Barrier Cost (\$)	Approx. Cost/Receptor(\$)	Considered Economically Feasible
R02	1	5	669	1,672,500	1,672,500	No
R04	1	5	253	632,500	632,500	No
R05	3	5	2544	6,360,000	2,120,000	No
R10	1	5	59	147,500	147,500	No
R18	1	5	28	70,000	70,000	Yes

Per MTO policy, although the noise caused by the recommended highway plan is ≥5 dB, noise mitigation is not feasible for:

- Receptors R03, R07, R08, R09, R11, R14, R15, R16, and R17, as these barriers do not meet technical feasibility requirements of reducing noise levels by a minimum 5 dB (see **Table 4.2**).
- Receptors R02, R04, R05 and R10, as barriers are not considered economically feasibility as the barrier cost per household exceeds the MTO rule of thumb 'ballpark' cost limit of \$100,000 per receptor (see Table 4.3).

Per MTO policy, a noise barrier at R18 appears to be warranted because:

- The increase in noise caused by the recommended plan at this location is ≥5 dB impact (see Table 4.1);
- At this location a noise barrier with a height of 5 metres would meet the minimum noise reduction requirement of 5 dB (see Table 4.2); and
- It is considered economically feasible because the barrier cost per household is less than the MTO rule of thumb 'ballpark' cost limit of \$100,000 per receptor (see **Table 4.3**).

The necessity for noise mitigation for receptor R18 is recommended for further exploration and examination during detail design once the horizontal and vertical alignment of the new highway has been developed in greater detail and the property acquisition process for this receptor is complete.

Noise mitigation recommendations at this stage of the project are preliminary in nature and should be reviewed further during the detailed design phase of this project and in consideration of the outcome of the property acquisition process.

5. Construction Noise

5.1 Municipal Noise Control By-Laws

The Township of Bonfield sets out noise restrictions and requirements in Noise Control By-Law 86-6. As with most municipal guidelines, the By-law is directed mainly at typical residential and commercial concerns and addresses those concerns in a qualitative manner. Relevant portions of the By-law are as follows:

- Operation of any item of motor vehicle, motorcycle, or any other vehicle whatsoever without effective muffling devices in good working order and in constant operation is prohibited.
- The discharge of exhaust from any steam engine, stationary internal combustion engine, motor vehicles or motorcycles, except through a muffler or other device which prevents loud or explosive noise is prohibited.
- Noise created by any vehicle which beats material, articles, or objects loaded on such vehicle in a manner calculated to disturb the repose of residence between 9:00 PM and 6:00 AM on the following day is prohibited.

The Township of Calvin does not currently have a noise By-law or policy.

In past projects, MTO has provided a public notice to all affected residents within a 500 metre radius of the project limits. The notice has been delivered approximately 3-4 weeks prior to overnight construction activities and included the following information:

- · General information regarding the anticipated construction activities
- The address (if available) or general area where the activity will take place
- The start and end date, and time of the activity
- The sources of the noise
- Methods of noise reduction
- A contact name/business or organization's name, address and phone number, email and fax.

Notification was also provided to the local councillors within the Project Area.

5.2 Construction Noise Control Recommendations

The Guide requires that the noise study documentation address the following for construction noise:

- Analysis of construction noise impacts and requirements for special provisions
- Identification of Noise Sensitive Areas
- Identification of municipal noise control By-laws
- Need to obtain noise By-law exemptions
- An explanation of any hardships to MTO caused by municipal noise control By-laws
- Construction noise complaint process

The severity of construction noise impact at Noise Sensitive Areas is dependent on various factors such as time and location of operation, size and concurrent use of equipment, and staging of construction. As equipment information is only available from the contractor awarded the construction contract, general recommendations relating to the management of construction noise are provided as follows:

 Adhere to applicable local By-laws. Where adherence to the local By-laws is not possible and mitigation is not feasible, an exemption should be obtained from the municipality before construction.

- Avoid construction activity during the night time, where not required, to reduce the potential impact of construction noise.
- Construction equipment noise emissions should comply with MOE guidelines NPC-115 and NPC-118.
- Contract documents provided to the contractor should contain general noise control measures to mitigate the noise impact at noise sensitive areas including two standard clauses regarding equipment noise:
 - Unnecessary noise caused by faulty or non-operating components must be addressed by regularly maintaining all equipment.
 - Duration of construction equipment idling is to be restricted to the minimum time necessary to complete the specified task.
- A noise complaint process may be set in place.
- Provide a public notice to all affected residents within a 500 metre radius of the project limits when overnight
 construction activities are to occur. The notice is to be delivered at least 3 weeks prior to the overnight
 construction activities and shall include the following information:
 - o General information regarding the anticipated construction activities
 - o The address (if available) or general area where the activity will take place
 - The start and end date, and time of the activity
 - o The sources of the noise
 - Methods of noise reduction
 - o A contact name/business or organization's name, address and phone number, email and fax.
- Provide notification to the local councillors within the Project Area.

Noise sensitive areas for the construction phase of this project will be the same as the noise sensitive areas included in the assessment of traffic noise impacts in the above sections.

A review of the Township of Bonfield Noise Control By-law (86-6) has been completed for sections relevant to this project. As with most municipal guidelines and By-laws, these By-laws are directed mainly at typical residential and commercial concerns. The Township of Calvin does not currently have a noise By-law or policy. The amalgamated relevant portions of the By-law are as follows:

- Operation of any item of motor vehicle, motorcycle, or any other vehicle whatsoever without effective muffling devices in good working order and in constant operation is prohibited.
- The discharge of exhaust from any steam engine, stationary internal combustion engine, motor vehicles or motorcycles, except through a muffler or other device which prevents loud or explosive noise is prohibited.
- Noise created by any vehicle which beats material, articles, or objects loaded on such vehicle in a manner calculated to disturb the repose of residence between 9:00 PM and 6:00 AM on the following day is prohibited.

The need for an exemption to the Township of Bonfield noise control bylaw, and confirmation that no such by-law is in place in the Township of Calvin should be determined during detail design for the project when a construction staging strategy has been developed. Construction infringing on the noise By-law should be discussed with the municipality and exemptions shall be sought if required.

An example noise complaint process is provided below:

- Any initial complaint from the public will require verification by the Ministry that all noise control measures to be applied are in effect. The Ministry will investigate any noise concerns, advise the contractor of any problems, and enforce its contract.
- Notwithstanding compliance with any noise control measures identified in the contract documents, a
 persistent complaint will require the Ministry to undertake a field investigation to determine noise level
 emissions. Where noise level emissions, for that construction equipment in use, exceed the sound level

criteria for construction equipment contained in the MOE Model Municipal Noise Control By-law, the Ministry shall require the contractor to comply with the sound level criteria where quieter alternative equipment is reasonably available. When this occurs, the Ministry shall pay the contractor for the costs incurred. Where a quieter alternative is not reasonably available, the equipment in use will be accepted.

6. Conclusions/Recommendations

The recommended plan involves improvements to Highway 17, upgrading it to a four lane controlled access freeway, from 2.2 km east of Highway 531 easterly and ending 8.0 km east of Highway 630. The recommended plan is expected to have a medium to high perceived noise impact at some noise sensitive receptors.

The necessity for noise mitigation, as presented in **Section 4.2**, is recommended for further exploration and examination during detail design for one receptor (R18) where initial analysis indicates that a barrier 5m high and 28m in length could address traffic noise levels from the widened /realigned Highway 17 at an approximate cost of \$70,000.

Noise from the construction of the road widening varies based upon a variety of factors such as time and location of operation, size and concurrent use of equipment, and staging of construction. Much of this information is currently unavailable; therefore general recommendations to minimize the impact of construction noise have been provided in **Section 5.1**.

7. References

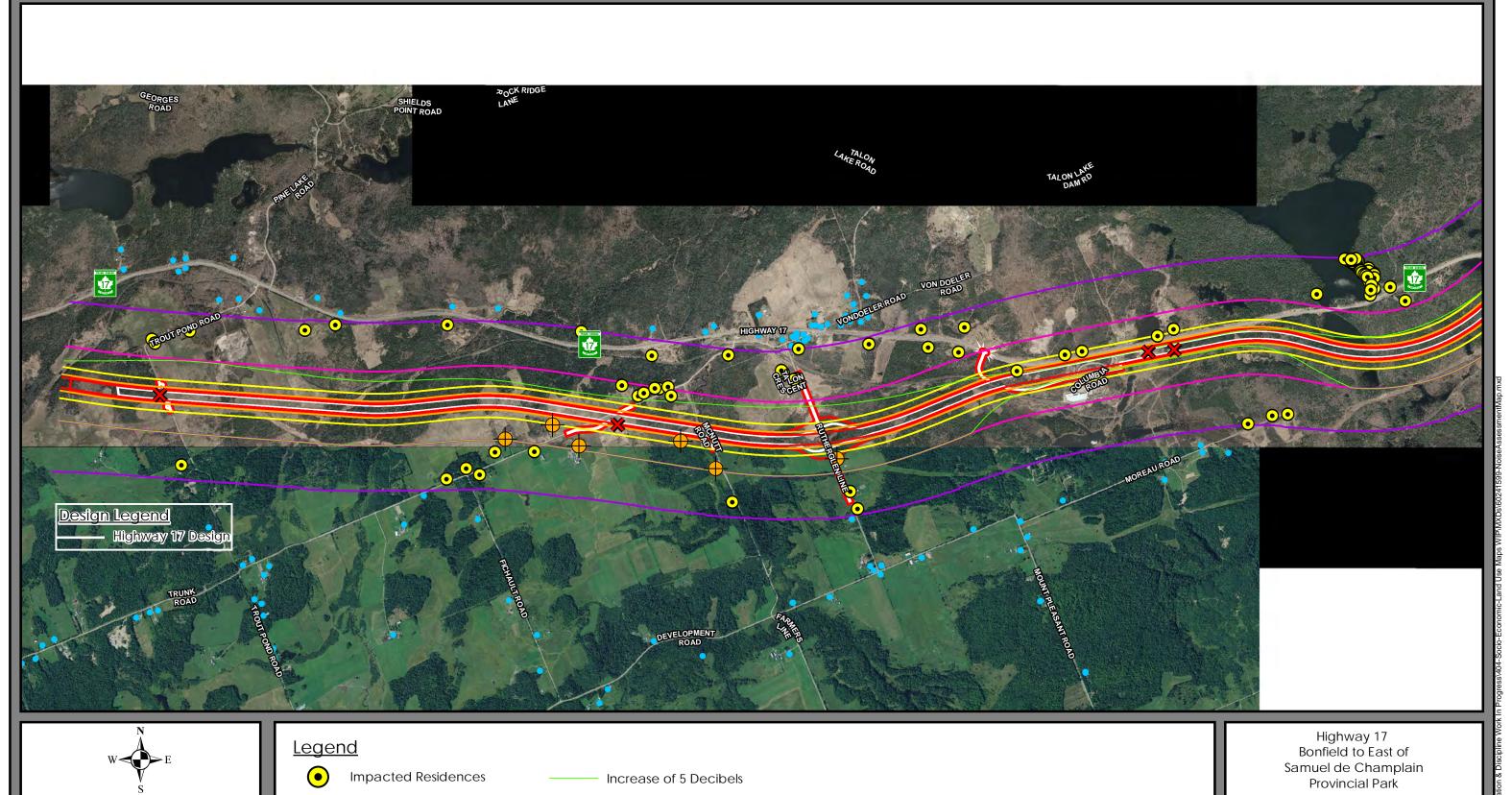
- 1. Ministry of Transportation Ontario, MTO Environmental Guide for Noise, October 2006.
- 2. ITE Journal, Traffic Volume Adjustments for Impact Analysis, James A. Bonneson, April 1987.
- 3. Ontario Ministry of the Environment, *Ontario Road noise Analysis Method for Environment and Transportation (ORNAMENT)*. Queen's Printer for Ontario, 1990.
- 4. Ontario Ministry of Environment, "Noise Assessment Criteria in Land Use Planning Publication LU-131", October 1997.
- 5. United States Federal Highway Administration, "FHWA Traffic Noise Model Version 2.5", April 2004
- 6. The Corporation of the Township of Bonfield, *By-Law No. 86-6 Being a By-Law to Control Noises in the Township of Bonfield*, 1986-05.

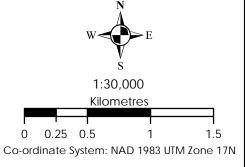
Appendix A

Appendix A: Recommended Plan (Please refer to TESR Appendix A)

Appendix B

Appendix B: Area of Investigation





Impacted Residences

Residents within area of 5 Decibel Level
5 Decibel Increase

Residential Removals

Residential Removals

Area Residences

Increase of 5 Decibels

Decibel Level

45 db

50 db

60 db

60 db

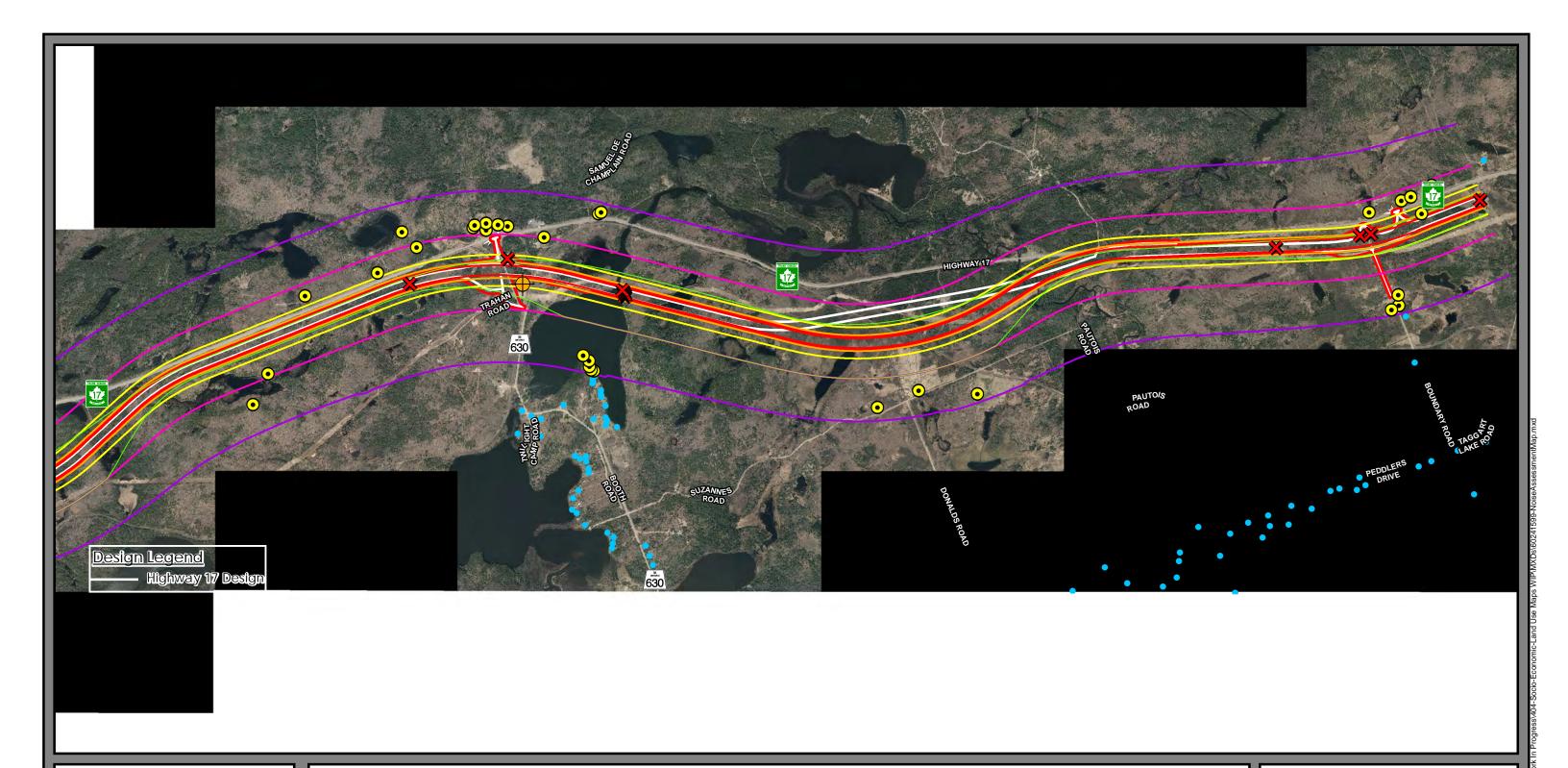
65 db

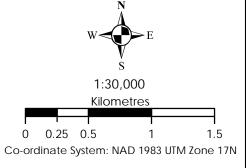
Noise Assessment Map

Ministry of Transportation Ontario December, 2013



60241599





<u>Legend</u>

Impacted Residences Increase of 5 Decibels Residents within area of

Decibel Level

45 db

5 Decibel Increase

50 db Residential Removals 55 db - 60 db Area Residences - 65 db Highway 17 Bonfield to East of Samuel de Champlain Provincial Park

Noise Assessment Map

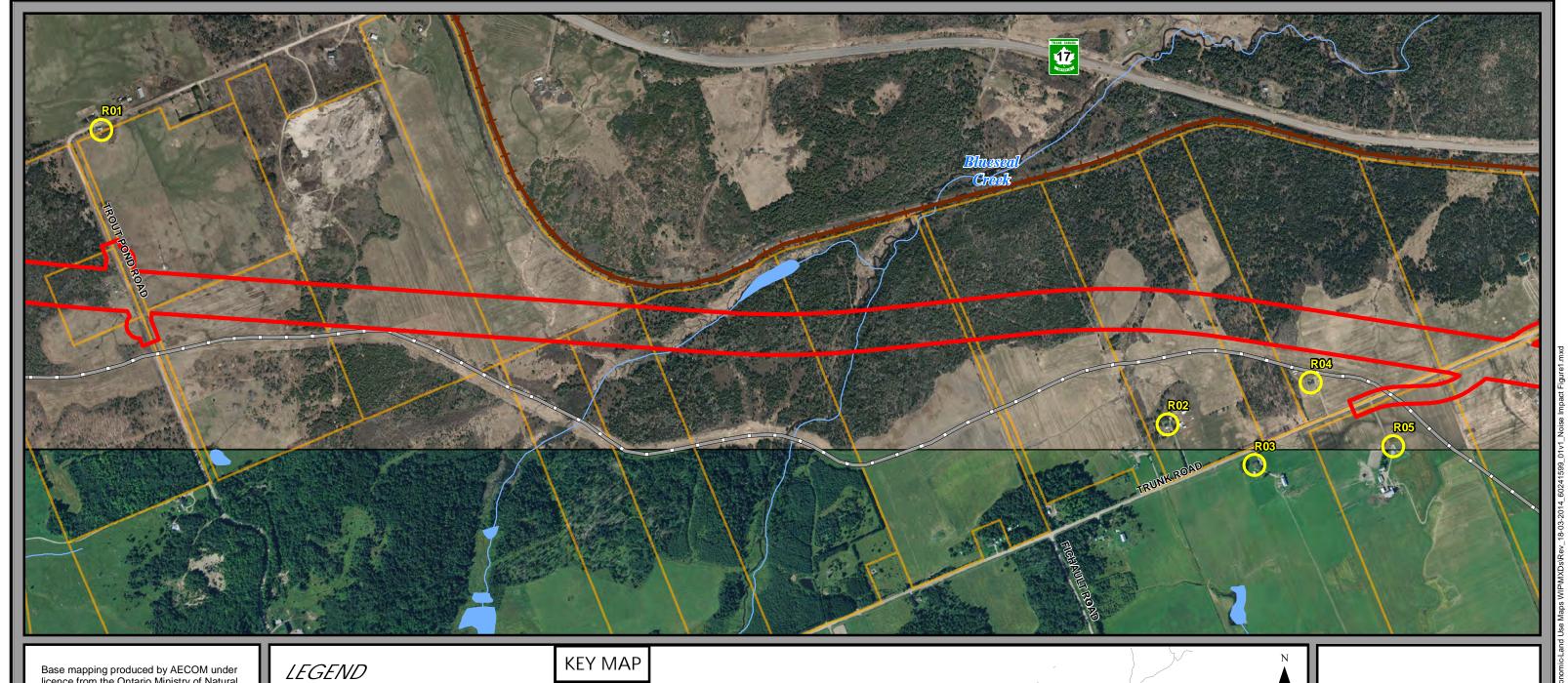
Ministry of Transportation Ontario December, 2013

AECOM

60241599

Appendix C

Appendix C: Detailed Assessment Receptor Locations



Base mapping produced by AECOM under licence from the Ontario Ministry of Natural Resources (MNR), Copyright© Queens Printer 2011. This licence does not constitute endorsement of this product by MNR or the Ontario Government.

Municipal Boundary

TransCanada Pipeline

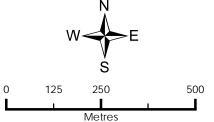
Noise Assessment Receptors

Route Footprint

Railway

Waterbody

Provincial Park



NAD 1983 UTM Zone 17N

This drawing has been prepared for the use of AECOM's client and may not be used, reproduced or relied upon by third parties, except as agreed by AECOM and its client, as required by law or for use by governmental reviewing agencies. AECOM accepts no responsibility, and denies any liability whatsoever, to any party that modifies this drawing without AECOM's express written consent.



Highway 17 Environmental Assessment

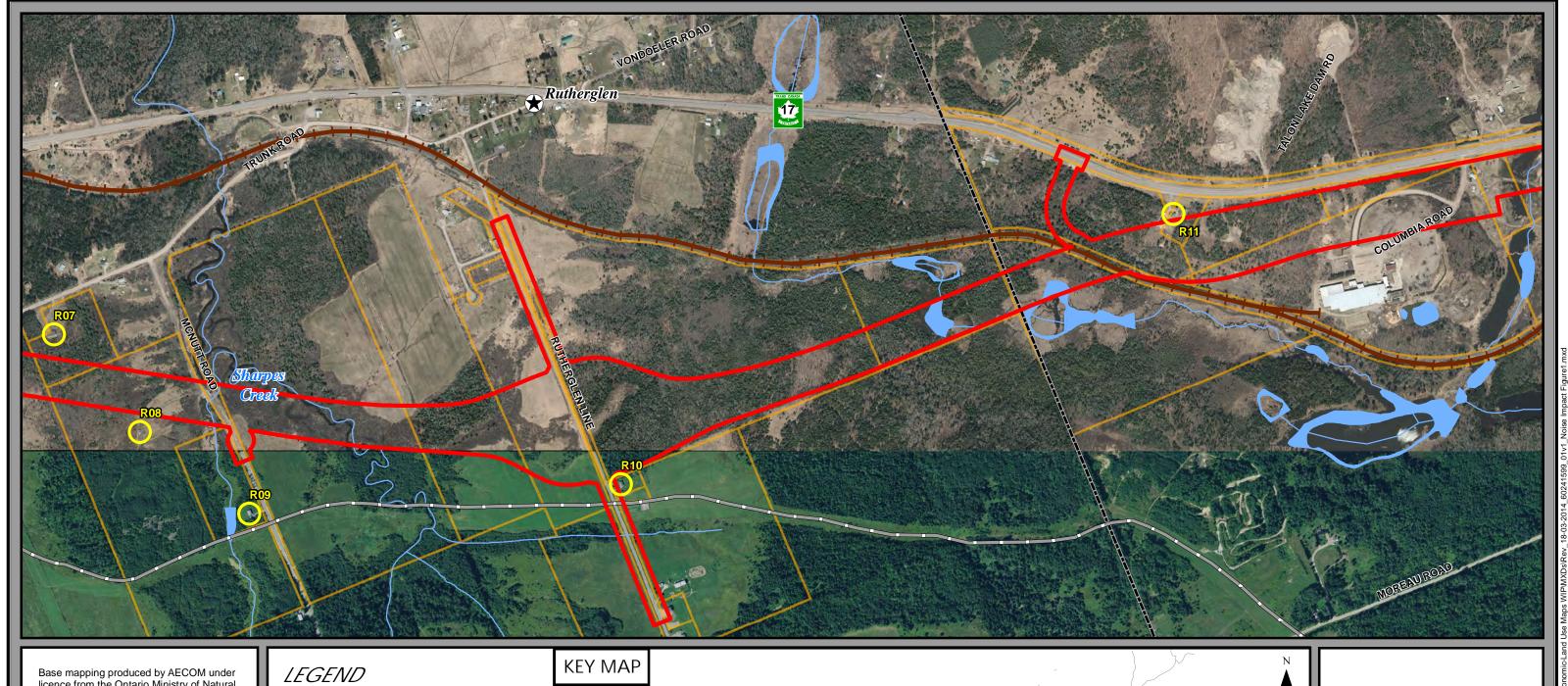
Noise Receptor Map: 1

Figure: 1

March, 2014 Project #: 60241599



.\60241599\400-Technical Information & Discipline Work In Progress\404-Socio-Economic-Land Use Maps WIPMXDs\Rev_18-03-2014_602.



Base mapping produced by AECOM under licence from the Ontario Ministry of Natural Resources (MNR), Copyright© Queens Printer 2011. This licence does not constitute endorsement of this product by MNR or the Ontario Government.

Municipal Boundary

TransCanada Pipeline

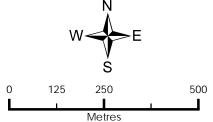
Noise Assessment Receptors

Route Footprint

Railway

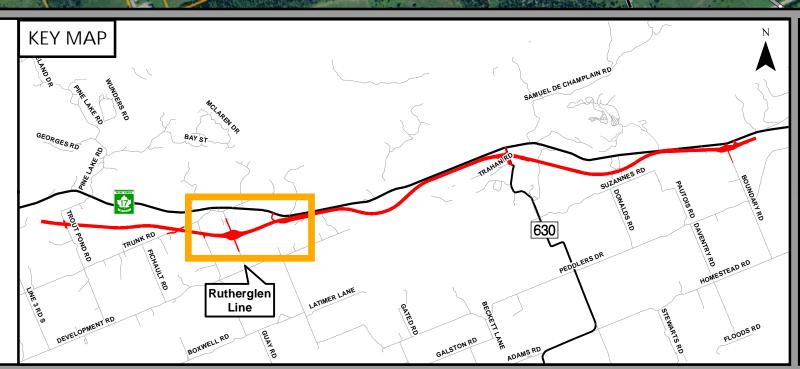
Waterbody

Provincial Park



NAD 1983 UTM Zone 17N

This drawing has been prepared for the use of AECOM's client and may not be used, reproduced or relied upon by third parties, except as agreed by AECOM and its client, as required by law or for use by governmental reviewing agencies. AECOM accepts no responsibility, and denies any liability whatsoever, to any party that modifies this drawing without AECOM's express written consent.



Highway 17 Environmental Assessment

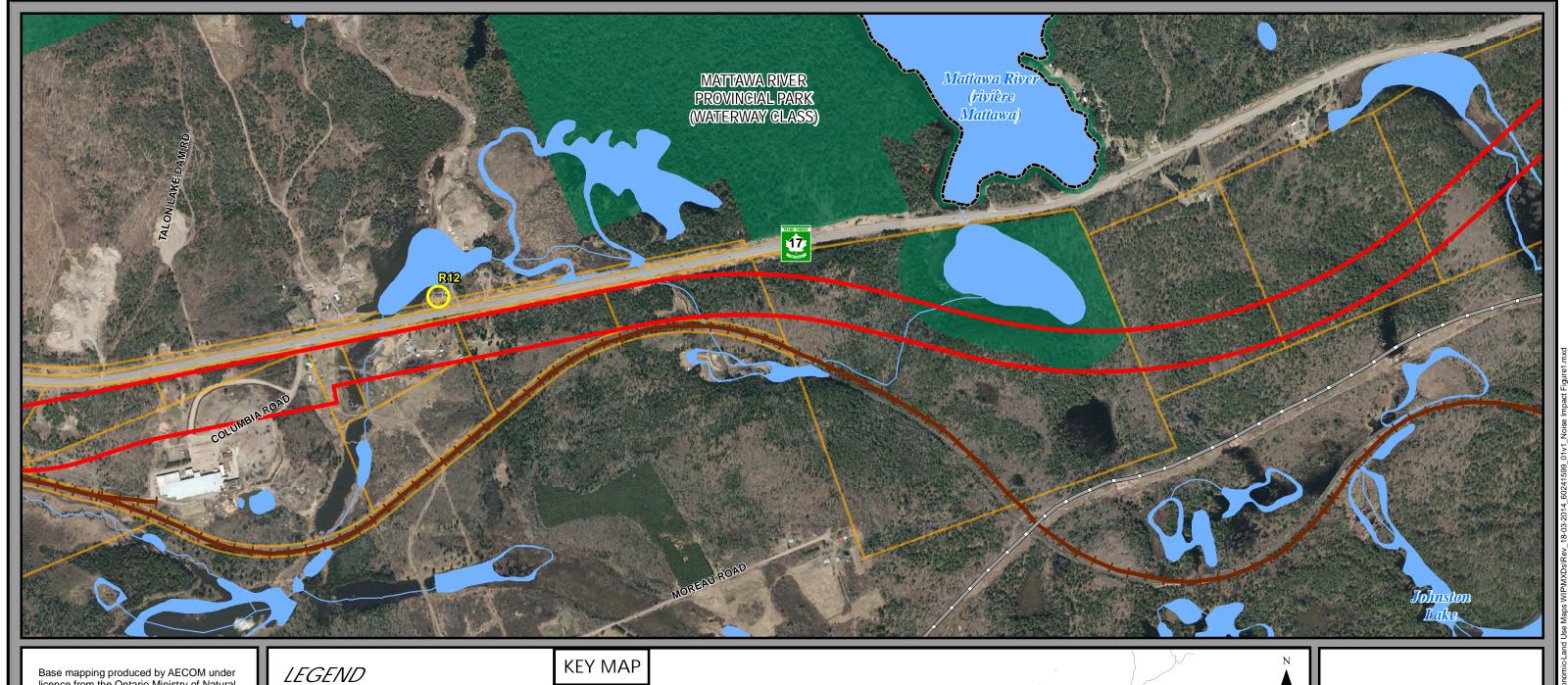
Noise Receptor Map: 2

Figure: 1

March, 2014 Project #: 60241599



241599\400-Technical Information & Discipline Work In Progress\404-Socio-Economic-Land Use Maps WIPMXDs\Rev_18-03



Base mapping produced by AECOM under licence from the Ontario Ministry of Natural Resources (MNR), Copyright© Queens Printer 2011. This licence does not constitute endorsement of this product by MNR or the Ontario Government.

Municipal Boundary

TransCanada Pipeline

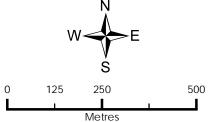
Noise Assessment Receptors

Route Footprint

Railway

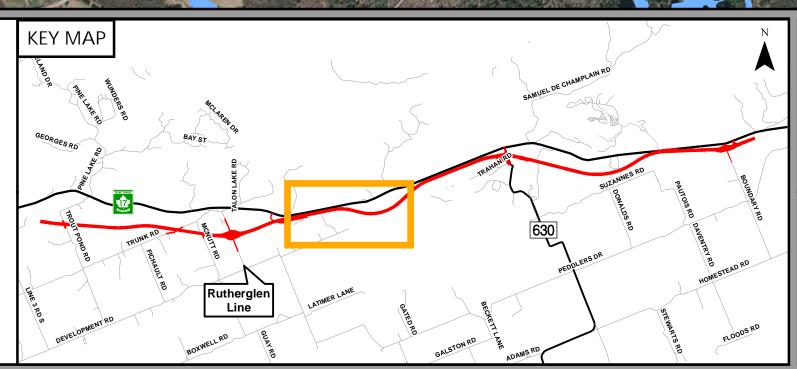
Waterbody

Provincial Park



NAD 1983 UTM Zone 17N

This drawing has been prepared for the use of AECOM's client and may not be used, reproduced or relied upon by third parties, except as agreed by AECOM and its client, as required by law or for use by governmental reviewing agencies. AECOM accepts no responsibility, and denies any liability whatsoever, to any party that modifies this drawing without AECOM's express written consent.



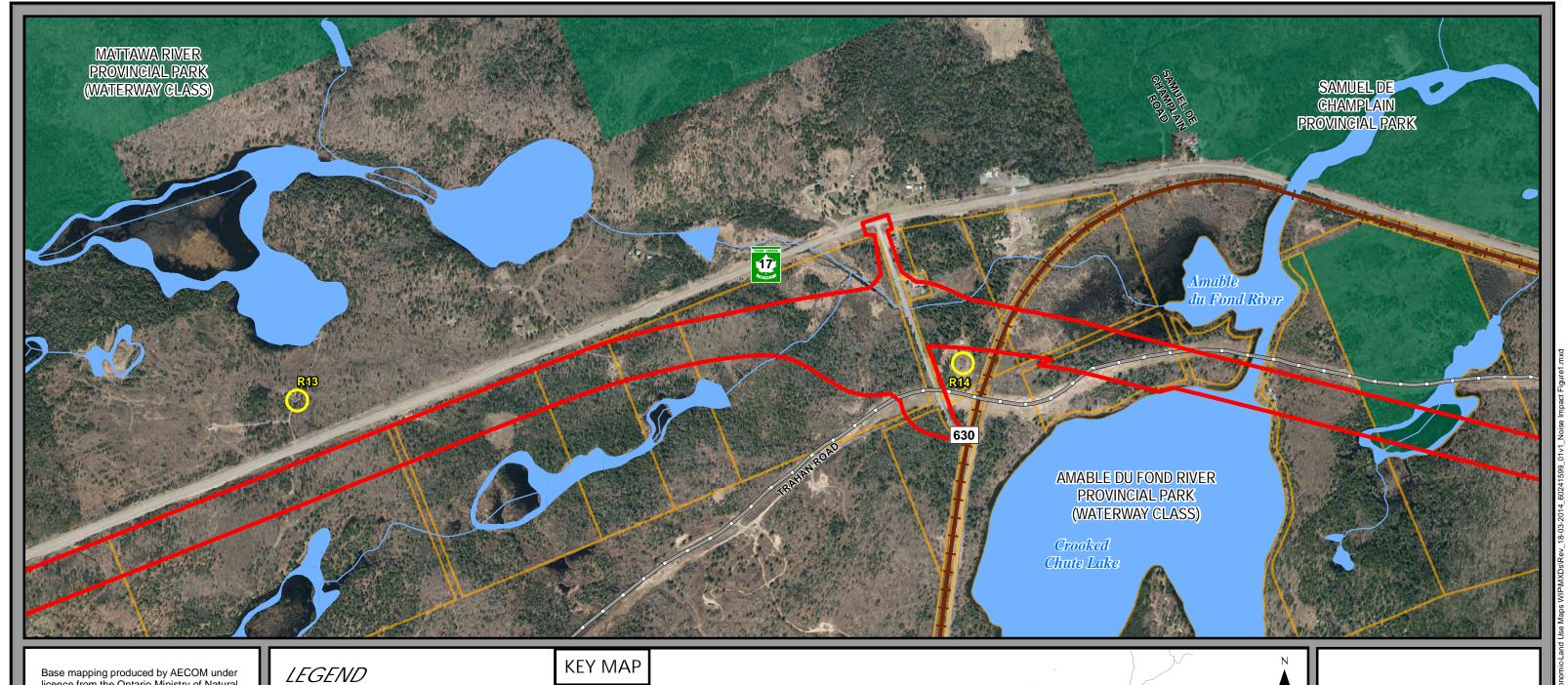
Highway 17 Environmental Assessment

Noise Receptor Map: 3

Figure: 1

March, 2014 Project #: 60241599

AECOM



Base mapping produced by AECOM under licence from the Ontario Ministry of Natural Resources (MNR), Copyright© Queens Printer 2011. This licence does not constitute endorsement of this product by MNR or the Ontario Government.

Municipal Boundary

TransCanada Pipeline

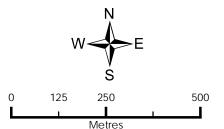
Noise Assessment Receptors

Route Footprint

Railway

Waterbody

Provincial Park



NAD 1983 UTM Zone 17N

This drawing has been prepared for the use of AECOM's client and may not be used, reproduced or relied upon by third parties, except as agreed by AECOM and its client, as required by law or for use by governmental reviewing agencies. AECOM accepts no responsibility, and denies any liability whatsoever, to any party that modifies this drawing without AECOM's express written consent.



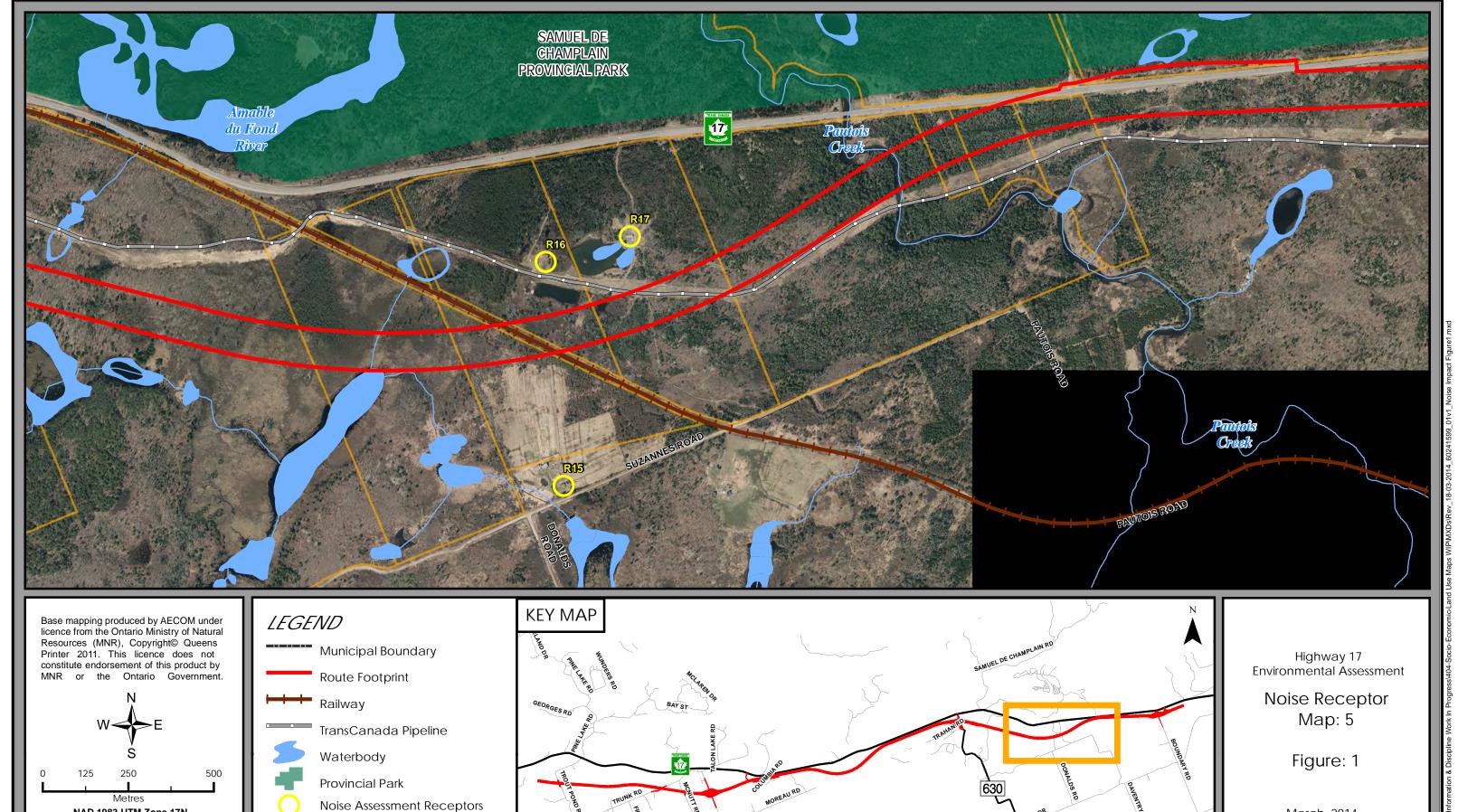
Highway 17 Environmental Assessment

Noise Receptor Map: 4

Figure: 1

March, 2014 Project #: 60241599

AECOM



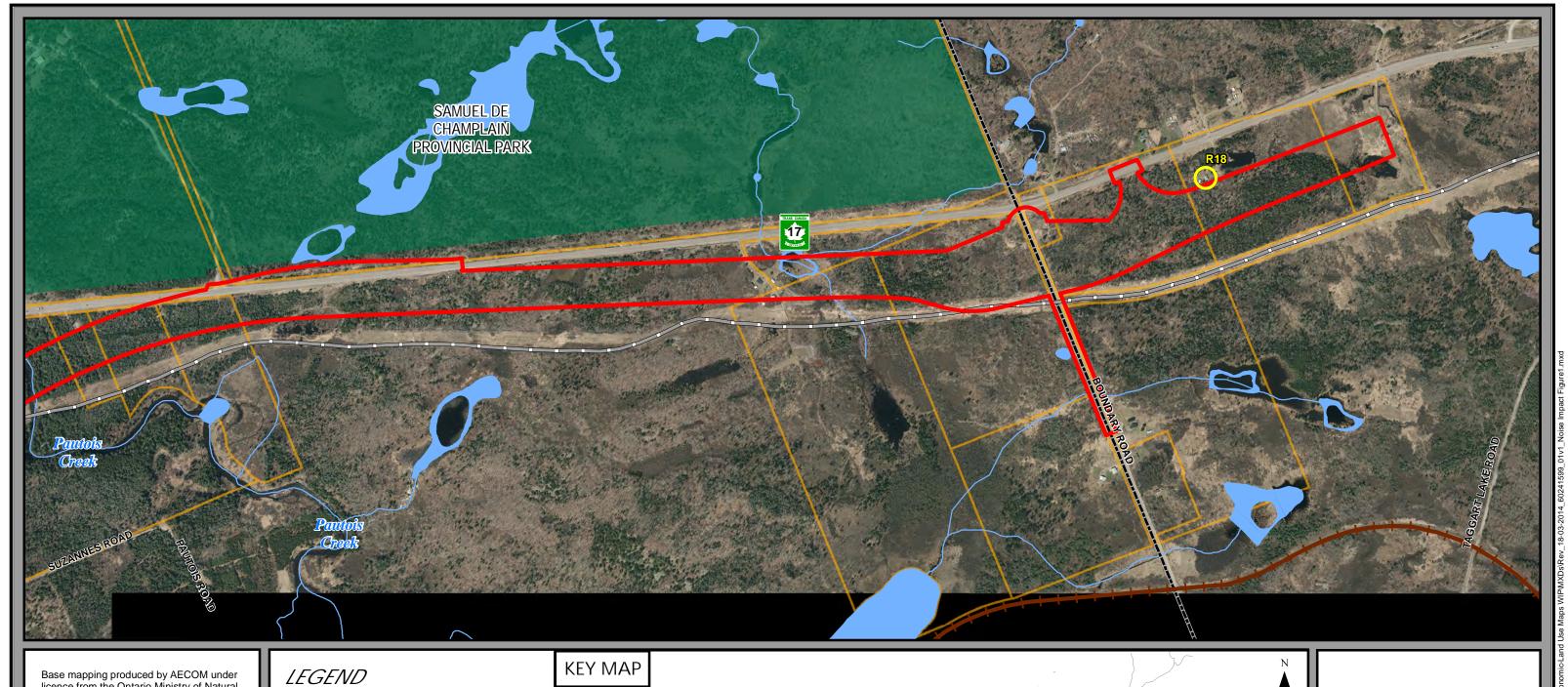
This drawing has been prepared for the use of AECOM's client and may not be used, reproduced or relied upon by third parties, except as agreed by AECOM and its client, as required by law or for use by governmental reviewing agencies. AECOM accepts no responsibility, and denies any liability whatsoever, to any party that modifies this drawing without AECOM's express written consent

NAD 1983 UTM Zone 17N

Rutherglen Line

March, 2014 Project #: 60241599





Base mapping produced by AECOM under licence from the Ontario Ministry of Natural Resources (MNR), Copyright® Queens Printer 2011. This licence does not constitute endorsement of this product by MNR or the Ontario Government.

Municipal Boundary

TransCanada Pipeline

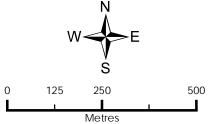
Noise Assessment Receptors

Route Footprint

Railway

Waterbody

Provincial Park



NAD 1983 UTM Zone 17N

This drawing has been prepared for the use of AECOM's client and may not be used, reproduced or relied upon by third parties, except as agreed by AECOM and its client, as required by law or for use by governmental reviewing agencies. AECOM accepts no responsibility, and denies any liability whatsoever, to any party that modifies this drawing without AECOM's express written consent.



Highway 17 Environmental Assessment

Noise Receptor Map: 6

Figure: 1

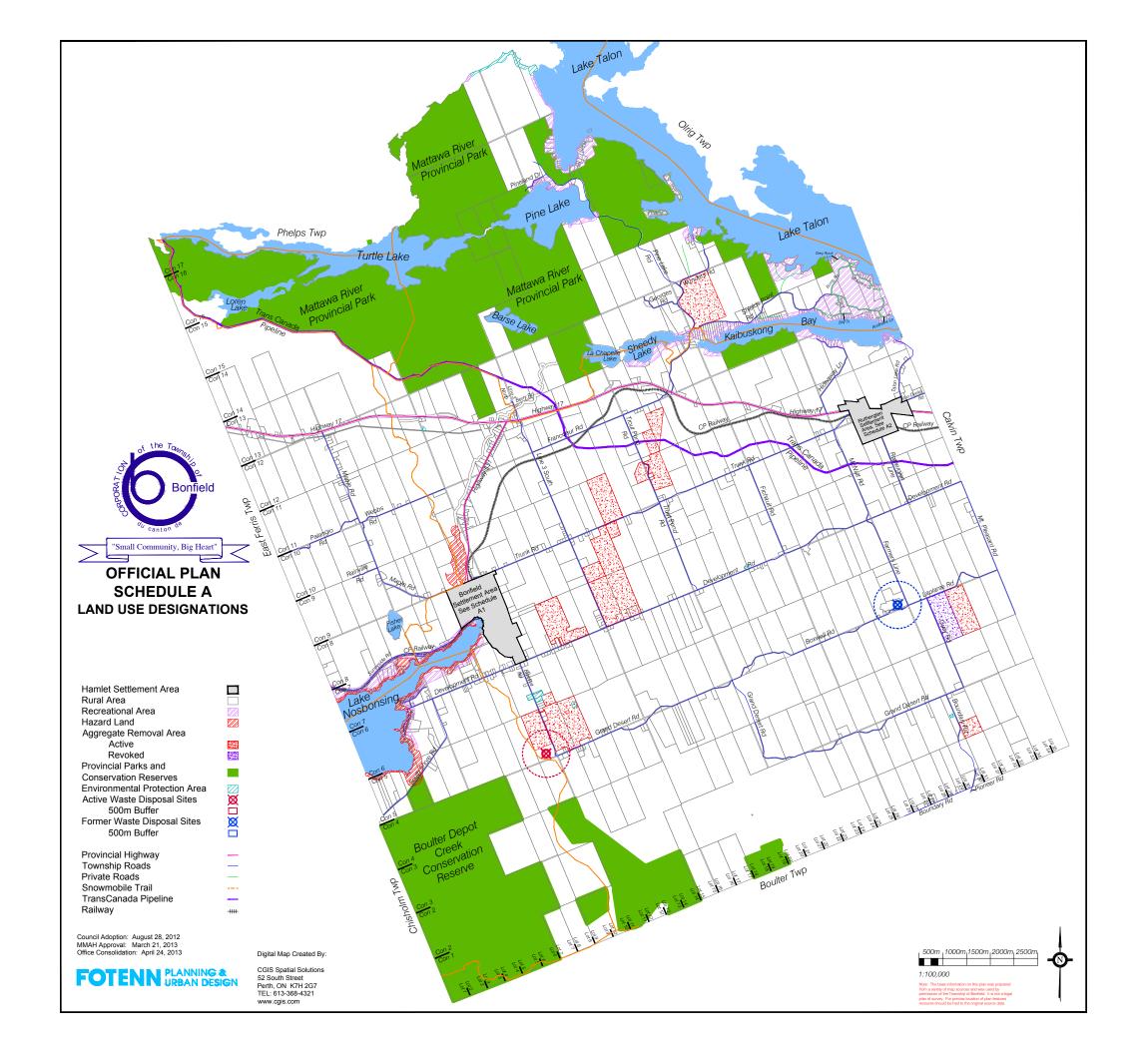
March, 2014 Project #: 60241599

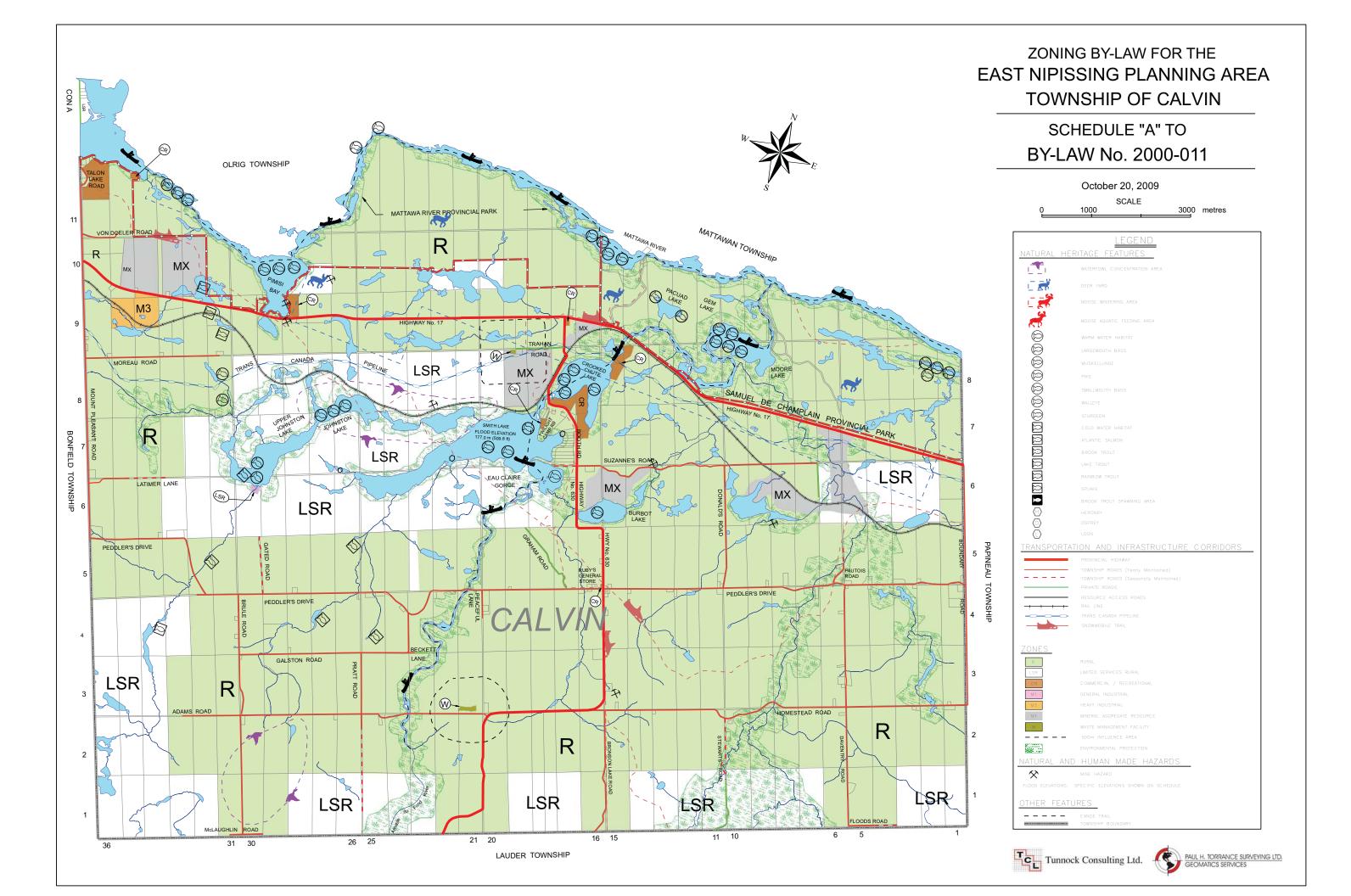


AECOM

Appendix D

Appendix D: Zoning Plan





Appendix E

Appendix E: Proposed Noise Barriers



Base mapping produced by AECOM under licence from the Ontario Ministry of Natural Resources (MNR), Copyright© Queens Printer 2011. This licence does not constitute endorsement of this product by MNR or the Ontario Government.

Municipal Boundary

TransCanada Pipeline

Noise Assessment Receptors

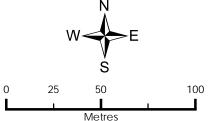
Recommended Barrier

Route Footprint

Railway

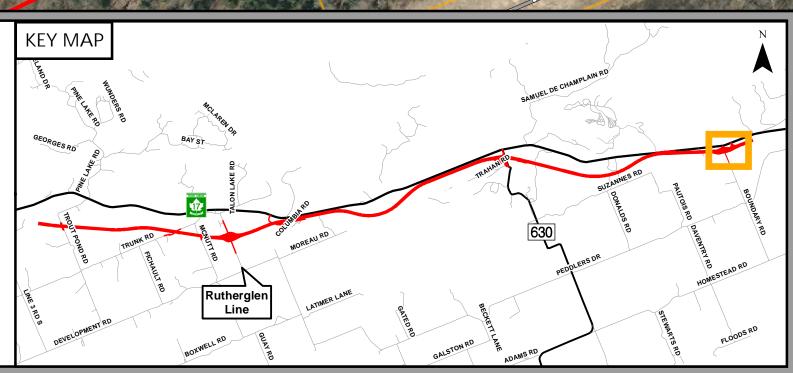
Waterbody

Provincial Park



NAD 1983 UTM Zone 17N

This drawing has been prepared for the use of AECOM's client and may not be used, reproduced or relied upon by third parties, except as agreed by AECOM and its client, as required by law or for use by governmental reviewing agencies. AECOM accepts no responsibility, and denies any liability whatsoever, to any party that modifies this drawing without AECOM's express written consent.



Highway 17 Environmental Assessment

Noise Receptor
Barrier Map

Figure: 2

March, 2014 Project #: 60241599



Appendix F

Appendix F: Traffic Data

		No Project		With Project					Road Only Parameters	ters
Source	Year	SADT	Year	SADT	%M.T. or #MT or %H.T. or #HT or Speed #Loc #Cars Limit (kph) Grade %	%H.T. or #HT or #Cars	Speed Limit (kph)	Grade %	Pave	Day/Night Split
Old Alignment	2035	10200			5.77	9.23	06	<2	1	85/15
New Alignment EB			2035	5100	5.77	9.23	100	7>	1	99/33
New Alignment WB			2035	5100	5.77	9.23	100	7>	1	99/33

Appendix G

Appendix G: Traffic Noise Calculations

20 8	8 rian Buras	March 13, 2014
PAGE	ENGINEER	DATE
Highway 17 - Rous Planning Borfast Essenty	60241999	0
PROJECT NAME	PROJECT NUMBER	BASE DRAMING

	ŝ.																											$\overline{}$	
	othy (db4)					. 998						. 460	. 298								. 592	. 992				. 9239	. 9238		
	ania LegDa) or (n) LegDn) (dB0)		45.43	44.79	48.132.0785	313207854		47.42	4826	3027	301	50.9441397	c 5.94413867		46.11	46.68	34.98	34.08	44.75	45.33	51.9710285	69710285		54.58	56.38	58.570838	13570828		
	or d Base of Barrier (ts) Boundon (rs)					Impact				262	262		mpact			٠	262	262				шрва					Impact		
	Redver out Ground (n) Beatler (t)		380	380				254	254	254	254				200	200	200	200	200	200				260	280				
	Elevation Change (e) Source Ground (m) Elevation (m)		288	288				249	249	18	18				248	248	220	280	249	249				252	282				
	Change (m)		2	2				40	40	3	6				ŽĮ.	22	9	9	£	=				00	**				
	Barter Receiver n) Detance (n)									216	215						182	182											
	Barrier Height (m)		٠							0	0						0	0						٠					
	1 Barr 92		٠							06	06						30	30											
Mah Brotan	\perp									16	8						.30	.30						٠					
	Source Receiver Dist (m)		397	84				318	280	318	280				398	348	398	348	386	348				141	108				
	Receiver Height (r) (m)		1.2	1.2				12	12	12	12				12	12	12	12	12	12				12	12				
	Surface Type		-	-				-	-	-	-				-				-	-					-				
	8 Dansity		٠	٠							٠					٠	٠	٠						٠	٠				
	No. Rows		٠	٠							٠					٠	٠	٠						٠					
	woods							٠			٠														٠				
	T0P0		9	6				3	9	4	4				9	3	4	4	e	3				9	6				
	95		8	8				8	8	8	8				-20	-20	8	30	8	06				06	06				
	91		ş	ş				8	8	16	16				8	8	œ	œ	8	8				8	ş				
	Leq Might (db.A)	٠			٠							٠																	
	Log (pilly) (dBly)	46			45		45					45		45							45		46			45			
	Base of Barier Elevation (no	٠												٠									٠						
	Receiver Gound Blevalion (nt)	280					256							092									980						
	Source Geornal Besellon (rs.)	٠												٠									٠						
	Bevation Change (s) (m)	٠																											
	Barrier Roceiver Distance (rs)																												
	Barrier Height (m)																												
	Barr 62																												
Mr. Broker	Barr 01																												
	Source Receiver Distr(m)	009<					>800							0094									0094						
	Receiver Height (r) (m)	1.2					1.2							1.2									1.2						
	Ground Surface Type	1					1							1									1						
	@ Density						٠																						
	No. Rows																												
	woods																												
	TOPO	1					1							1									1						
	92	06					90							06									06						
	91	-90					-90							06-									06-						
	SOURCE	Old Algriment	New Alignment WB	New Algrment EB	Total		Old Algoment	New Algrment WB1	New Algrman EB 1	New Algrment WB2	New Algrman EB2	Total		Old Mignment	New Algriment WB1	New Algement EB1	New Algement WBZ	New Algement EB2	New Algrment WB3	New Algement EB3	Total		Old Migment	New Algoriant WB	New Algrment EB	Total			
	RECEIVER	1001					R32			Used average height across viewing angle for Barrier Base Bevafon	Used average height across viewing and e for Barrier Base Elevaton			PD3			Used average height across viewing angle for Barrier Base Ellevaton	Used average height across viewing angle for Barrier Base Elevation					R04						

∞	1	
2 0	Brian Bunes	March 13, 2014
	85	
PAGE	BYGINEER	DATE
Highway 17 - Rouse Planning Borril ad Easterly	602/1/399	
PROJECT NAME	P ROJECT NUMBER	BASE DRAWING

			1	1	1			1		1	1													1			
Leq(Mgt) (dbA)			٠				٠						٠											٠			
LegDay) or Legg (rk) (dbb)		47.35	48.34	50.8834486	5.88344863		50.12	48.79	52.5160153	2.20601527			43.53	40.6	38.62	37.04	45.82	43.5	50.291.4672	6.29146724		29159	56.51	58.31 13.84	13311384		
Bare of Berrier Beuden (rs)					Impact					mpact			254	254	992	992	253	253		mpsct					mpact		
Receiver Ground Beauton (ts)		252	282				253	253					2.48	2.48	248	248	248	2.48				245	246			ì	
Bevation Change (e) Bource Ground (m)		253	263				263	253					253	263	250	250	246	246				246	346				
Elevation Change (e)			-										9	9	2	2	2	2									
Barter Receiver Detance (n)													83	63	83	83	8	8									
Barrier Height (m)													0	0	0	0	0	0									
Barr 02													46	-46	45	45	08	06									
Wah Project Barr 81													8	6.	9-	9-	16	16									
Source Receiver Dist (m)		283	248				182	219					88	138	68	126	8	138				112	16				
Receiver Height (r)		1.2	1.2				12	12					12	12	1.2	1.2	12	12				1.2	1.2				
Ground Surface Tyce							-	-					1	1	1	1	-					1	1				
® Dereity																											
No.Rows																											
N SOOOM																											
901	1	9	6				-						4	4	4	4	4	4									
65		8	8				8	8					-45	-45	46	46	8	96				90	90				
10		8	ş				8	8					8	8	9	9	8	16				8	8				
(di N																											
(agp)	46			45		90.31			90.31			46							45		45			45			
Base of Barter Log El exten (nt) (c									8										-								
Receiver Geound Base of Bavildon(m) Base						263						248									245						
Rec Beute Georn! Ge Beuten (n)						246 2																					
Elevation Change (s) Source (m) Elevat						8 2																					
ser Change																											
Barrier Roceiver L(m) Debarron (n)																											
Barier Heighton)	ľ																										
Hect 81 Barr 82																											
No Project iver m) Berr 81																											
We Source L(r) Receiver	>900					407						009x									009×						
Ece Height (r)	_					1.2						1.2									1.2						
Ground Surface alty Type						1						-									-						
we 8 Density																											
DS No. Rows																											
woom																											
0401	1					3						-															
91 92	<u> </u>					-90						06 06-									06 06-						
		ant WB	ant EB	_			art WB	Banac	_				art WB1	ort EB1	art WB2	9rt EB2	int WB3	ert EB3	_			art WB	and EB	_			
SOURCE	OdAlignment	New Algement WB	New Algrment EB	Total		OldAlgment	New Algriment WB	New Algranert EB	Total			Old Migment	New Alignment WB1	New Algrmort EB 1	New Algement WIIZ	New Algrand EB 2	New Algrment WISS	New Algrment EB3	Total		OldAlgnmant	New Algriment WB	New Algriment EB	Total			
RECEVER	R36					Pa3-6						P077			Used average height across viewing angle for Barrier Base Elevator	Used average height across viewing angle for Barner Bas e Elevation					P33-8						

80		_
8 8	Brian Bures	March 13, 2014
PAGE 3	ENGINEER	DATE
Highway 17 - Rouse Pluming Borfleds Easterly	60241599	
PROJECT NAME	PROJECT NUMBER	BASE DRAMING

Г	Leq (Ngh) (dbh)																						
	LeqDay or L		47.5	4852	51,0501765	6.0501765		51.88	63.39	55.7105995	10.7109986		64.79	62.18	66.638.4865	.61848552		55.23	52.98	57.259-4094	-7.0405906		
	Base of Barrier Lo Beuden (11) Leq				-10	Impact 6.1				88	Impact 10				99	Impact 7.6				52.	mpsc -7.		
	Recaver Ground Base Bession (tr) Be		23.7	23.7		-		241	241		-		257	257		-		221	221		-		
	Bource Ground G Bavation (n) Bea		238	238				346	246				236	236				219	219				
	Change (e) Sour (m) Box							10	9				22	22				2	2				
	Barser Be Receive Cha Distance (n)																						
	Barrier Res Height (m) Dean																						
	Barr 62 Heigi																						
	Wah Project war m) Barr 61																						
	or Source (i) Receiver Det (m)		277	240				185	147				46	82				46	134				
	d Receiver e Height(r) (m)		1.2	1.2				12	12				12	1.2				1.2	12				
	Surface Type							-	٠				٠	-				1	1				
	rs ® Dansity			٠					٠				٠						٠				
	8 No. Rows								٠				٠										
	woods		٠						٠				٠										
	Olo Tole		6	6				6	9				9	9				9	9				
	95		8	8				8	8				8	8				06	06				
	91		ş	ş				ę	8				8	8				8	8				
	Les Pligré (di A						٠																
	(Agp) (Agp)	46			45		45			46		59.07			40'69		643			643			
	Base of Barier Elevation (n)						٠																
	Receiver Gound Blevalon (n)	233					241					257					122						
	Bouto Gound Beatlon (rs)											255					230						
	Elevation Change (s) Source Geound (m) Benefici (n)											2											
	Barter Roceler Distance (n)																						
	Barier Height(m)																						
	Barr 92																						
	No Project Barr 81																						
	Source Receiver Distr(m)	>800					>900					92					38						
	Receiver Height (r) (m)	1.2					12					1.2					1.2						
		1										-											
	Ground Surface & Density Type																						
	No. Rows																						
	woods																						
	W W	1										3					3						
	1 1						90					06					06						
	10	-90					-90					06-					-30						
		3918	rt WB	88			30th	rt WB	ant EB			nert.	ert WB	3rt E8) Mile	er we	90 H				
	SOURCE	Old Algriment	New Algrment WB	New Algement EB	Total		Old Algriment	New Algriment WB	New Algrand EB	Total		Old Migment	New Algriment WB	New Algoment EB	Total		Old Migment	New Algriment WB	New Algrand EB	Total			
	RECENER	609					R10					III					R12						

8		
4 0¢	8	March 13, 2014
PAGE 4	ENGINEER	<u>u</u>
ρĄ	BYGI	DATE
Highway 17 - Roude Planning Bortfield Easterly	660 tr 700 0	
PROJECT NAME	PROJECT NUMBER	BASE DRAWING

	(ABA)																						
	helps) (ve) (be)		60.89	49.6	63.3030216	-3.3769784		56.62	59.1	61.0449585	12.9349685		47.17	47.65	50.426928	5.42692803		53.95	53.05	56.5390911	.87909112		
	Base of Barriar Lu Bevadon (rs) Luc				53	Impact -3				61	Impact 12				36	impact 5.4				26	impact 7.1		
	Redur Ground Bas Bouldon (19) Big		218	218				187	187				191	191				187	187				
	nce Ground author (nt) Bu		220	220				193	193				198	198				196	196				
	Elevation Change (a) Source Ground (m) Benation (n)		2	2				9	9				- 4					11	11				
	Burter E Receive CP Detance (nt)																						
	Barrier Height (m) Di																						
	Ват 62																						
10000																							
1	Source Receiver Dist (m)		181	218				8	20				441	409				183	238				
	Receiver Height(r) F (m)		1.2	1.2				12	12				12	12				12	12				
	Ground Surface Type			1				1	1				1	1				1	1				
	® Dansity																						
	No.Rows																						
	WOODS																						
	0401		6	9				3	3				3	3				3	3				
	95		8	8				8	8				8	8				06	06				
	10		ş	8				8	8				8	8				8	8				
	Less Prigrés (db.Ps																						
	(ABA) (ABA)	98.68			8.8		48.11			48.11		46			45		48.08			48.66			
	Base of Barler Elevation (nt)																						
	Receiver Geound Blevation (nt)	218					187					181					187						
	Sarre Geund Beutlen (rs)	221					190										196						
	Davation Change (iii) Save Gound (ini) Beaton (in)	3					3										1						
	Barrier Roceiver Distance (rs)																						
	Barisr Height(m)																						
	Barr 92																٠						
1	Barr 01																						
	Source Receiver Disk(m)	1112					303					0094					318						
	Receiver Height (r) (m)						12					1.2					1.2						
	Ground Surface Type	1					-					1					1						
	® Density	٠					٠					٠											
	No. Rows	٠					٠					٠					٠						
	WOODS																						
	70PO	9					e					·					3						
	95	96					96					06					06						
	91	06-					-90					06-					06-						
	SOURCE	Old Algriment	New Algement WB	New Algornant EB	Total		Old Algoment	New Algrand WB	New Algoment EB	Total		Old Algoment	New Algrand WB	New Algoment EB	Total		Old Algoment	New Algrand WB	New Algrand EB	Total			
	RECEIVER	R13					R14					R16					R16						

5 % 8	Brian Butwa	March 13, 2014
PAGE	ENGINEER	DATE
Hgway 17 - Roza Plarring Borfield Essistry	600241599	
PROJECT NAME	PROJECTNUMBER	BASE DRAMING

	Leq (Ngt) (dBA)											
	red(by) (4gb)		55.08	54.11	67.622251	8.02232513		60.54	56.13	61.8825458	5.44254584	
	Beaton (rs)					Impact					mpact	
	Receiver Ground Beutlen (tr)		188	188				218	218			
	Source Ground Blevation (m)		201	201				219	219			
	Bevation Change (e) (m)		63	63				1	ı			
	Barter Receiver Detarce (n)											
	Barrier Height (m)											
_	Ват Ө2											
With Project	Barr 91		٠	٠					٠			
	Source Receiver Dist (m)		281	217				4	28			
	Receiver Height (r) (m)		1.2	1.2				12	12			
	Ground SurBos Type		,	,				-				
	® Density		٠	٠				٠	٠			
	WOODS No. Rows		٠	٠					٠			
			٠	٠					٠			
	TOPO		6	6				6	3			
	95		8	8				8	8			
	91		8	8				ę	ę			
	(db.)				٠		٠			٠		
	or Log pate)	49.61			49.61		98.44			98.44		
	Base of Barier () Elevation (nt)						٠					
	Receiver Gound b) Bevillon (n)	188					218					
	a) Sarre Geund Beatlon (n) E	186					219					
	Change (s) 8 (m)	2										
	Barrier Roceiver 1) Distance (n)	٠					٠					
	Barier 2 Height (m)											
ŭ	1 Barr 92											
No Project	Barr 81						٠					
	y Source y) Receiver Distr(m)	236					106					
	5 Receiver e Height (r) (m)	1.2					1.2					
	Ground Surface ity Type						1					
	ws ® Density											
	28 No. Rows											
	MOOO8											
	TOPO	3					9					
	1 62	06 0					06 0					
	91	06-	o.				06-	6	6			
	SOURCE	Old Algrand	New Algement WB	New Algement EB	Total		Old Mignisht	New Algriment WB	New Algranant EB	Total		
	RECEIVER	R17					R18					

Mitigation Calculations

PAGE 6 OF 8	ENCINE ER Brian Bulnos	DATE March 13, 2014
Highway 17 - Rouse Planting Borthald Easterly	00241599	
PROJECTNAME	PROJECT NUMBER	BASE DRAWING

(cBA)																																			
Legithr) (dBV)		42.26	41.53	3027	30.1	5.203 19.28	7409-4592		40.95	36.86	34.98	34.66	43.81	37.92	7.2106722	7603528		49.86	50.67	3.2941567	527670587		42.83	42.29	5.5788875	530476116		41.85	39.00	38.38	34.67	46.72	43.38	49.5632482	0.72821904
Base of Buriar Beuden (rs.). L.		282	252	262	262	-	Reduction 5		252	252	262	262	249	249	-	Noise Reduction		257	12		Noise Beduction		254	84	4	Notes Baduction		84	84	256	256	263	263		Notes Reduction
Rectiver Ground Beadon (%)		254	254	254	254				260	260	260	260	260	280				200	200				262	262				248	248	248	248	2.48	248		
Source Ground Baration (m)		249	616	251	182				248	248	092	250	549	249				251	251				253	253				253	253	250	250	2.45	245		
Elevation Change (e) (m)		vo.	9	6	6				22	22	06	0,	Į.	F									1	-				9	9	2	2	2	2		
Barter Receiver Distance (m)		245	245	216	216				340	340	182	182	344	344				ĸ	ß				212	212				8	8	8	63	63	63		
Barrier Haight (m)		10	9	0	0				9	40	0	۰	10	40				40	10				9	10				9	40	40	10	9	9		
Barr 02		45	45	80	08				-20	-20	30	30	06	06				09	09				90	98				46	46	45	48	8	89		
Migated Barr 81		8	9-	19	16				8:	8:	.30	-20	30	30				9	09-				-90	8				96-	96-	45	46	46	46		
Source Receiver Dist (m)		318	280	318	280				382	348	382	348	382	348				244	108				283	246				8	126	68	126	68	126		
Receiver Height (r) (m)		1.2	1.2	12	12				12	12	12	12	12	12				12	1.2				1.2	12				1.2	1.2	1.2	1.2	1.2	1.2		
Ground Surface V									-	-		-	-	-				-	-				,	-				-	-	-	-		-		
As @ Density																								•											_
DS No.Rows																			٠					•											\dashv
sgoow o											٠												٠	•									•		4
0401		4	4	4	4				4	4	4	4	4	4				4	4				4	4				4	4	4	4	4	4		_
92		16	16	8	8				-20	-20	30	30	06	06				08	08				08	8				48	45	45	46	06	06		_
90		ş	00-	10	10				ą	ą	œ.	8	8	8				ė.	8				-90	-90				99	90	8	46	46	46		_
(day (all) (day)			. 8			1397						. 9			. 5820				. 9	. 9298			. 91		4486									4672	-
		47.42	- 48.38	36.2 30.27	30.1	50.9441397			. 46.11	. 45.68	262 34.98	382 34.66	. 44.75	. 45.33	51.9710285			- 5458	. 98.36	59:5703626			. 47.35	- 4834	50.8834486			4 43.53	4 40.6	9862	8 37.04	3 45.82	3 435	90.2914672	_
Receiver Base of Banker Georgia Banker (np.			254	254 38	254 38				. 980	. 380	380 38	360 26	. 092	. 980				- 920	380				252	. 282				254	254	248 256	248 256	248 253	248 253		_
Rec Sarre Geunst Divide Beudich (19)		249 2	249 2	251 2	251 2				248 3	248 3	250 3	250 3	249 3	249 3				252 3	252 3				283 2	233				263 2	263 2	220 2	220 2	246 2	246 2		
Elevation Change (a) Source (m) Beve		10	9		6				12 2	12 2	10	10	11										,	-				10	10	2	2	2 .	2 2		_
Barser Els Roceiver Cha Distance (n)				215	215						182	182																63	63	63	63	63	63		
Barier R Height(m) Des				0	0						0	0																0	0	0	0	0	0		_
Barr 62 Ho				90	8						8	93																ş	9.	8	45	8	8		
Urmitjated Barr 01				45	46						-20	-20																8	8	ń	ą	46	8		_
Source Receiver Dist(m)		318	280	318	380				382	348	386	348	386	348				144	108				283	246				68	128	68	138	89	126		
Receiver Height (r) (m)		12	1.2	12	12				17	175	1.2	175	1.2	1.2				12	1.2				1.2	1.2				1.2	1.2	1.2	1.2	1.2	1.2		
Ground Surface Type		-	1		-				-	-		-	-	-				-	-				1	-				-	-	-	-				
@ Densky																																			
No. Rows				٠																															
woods																																			
0401		6	3	4	4				8	8	4	4	9	9				e	e				9	6				4	4	4	4	4	4		
92		46	45	90	90				-20	-20	30	30	06	8				8	8				06	8				¥	¥	8	8	8	8		
91		-90	-80	45	6				90	90	-20	-20	30	30				08-	08-				-80	08-				90	ą	ş	¥	46	9		
SOURCE	OdAlgrimm	New Algrment WB1	New AgrmentEB1	New Algement WB2	New Algrment EB2	Total		Old Algoment	New Algoment WB1	New Algranant EB 1	New Algranert WB2	New Algranart EB 2	New Algoment WB3	New Algrownt EB3	Total		Old Algoment	New Algnment WB	New Algrand EB	Total		Old Algriment	New AfgrmentWB	New Algoment EB	Total		Old Algrment	New Algrand WB1	New Alignment EB1	New Algriment WB2	New Alignment EB2	New Algrand WB3	New Algnment EB3	Total	
RECEIVER	P022			Used average height across viewing angle for Barrior Base Elevation	Used average height across viewing angle for Barrier Base Elevaton			R03			Used average height across viewing angle for Barrier Base Elevation	Used average height across viewing angle for Barrier Base Elevation					R04					ROS					ROT			Used average height across wowing angle for Barrier Base Elevation	Used average height across viewing angle for Barrier Base Elevation				

Mitigation Calculations

PAGE 7 OF 8	ENGINEER Brian Burns	DATE March 13, 2014
Highway 17 - Rouse Planning Borfast Essionity	602.41.599	
PROJECT NAME	PROJECT NUMBER	BASE DRAWING

	Leq(Ngr) (dBA)																											\exists
	Legibly) or Legi				54564943			47.5		1.0601765	0				3042					0.6884865								_
	Base of Barrier LegDb Beaden (n) LegDre		243 50.36	243 52.49	54.56	Noise 3.74678989 Reduction		234 47	234 48.52	51.060	Noise 0 Reduction 0		241 46.84	241 48.32	50.653042	Noise 5.05759557 Reduction		242 64.79	242 6218	66.68	Noise 0 Reduction 0		185 54-49	185 99.1	60390255	Noise 0.85471352 Reduction		-
	Red or Base of Beat Beat		246 2	246 2		Red		237 2	237 2		Redi		241 2	241 2		Red		257 2	257 2		Redi		187 1	187		Nc Pards		
	Source Ground Shoel		246 2	246 2				238 2	238 2				246 2	246 2				235 2	235 2				193	193 1				-
	Change (e) Source							-	1 3				10	9				21	21				9	9				-
	Receive Char Detarce(n)		39	39				204	204				17	13									30	8				
	Barrier Re Height (m) Deza		10	10				9	6 2				10	10				10	10				9	10				-
	Barr 92 Haic		06	90				06	90				09	09				06	06				90	06				
			8	8				8	90				8.	8				06-	-90				-80	-30				-
1	Source Receiver		112	16				277	240				185	147				ń	20				ž.	2				_
	Receiver S Height(r) Re		1.2	1.2				12	12				12	12				12	12				12	1.2				
	Ground Re Surface He		1	1				1	1				1	1				-	1				1	1				
	S Dansity	_																										
	No. Rows																											٦
	NOOON																											
	0407		2	2				4	4				4	4				4	4				4	4				
	95		8	8				8	8				8	06				06	06				90	06				
	91		8	8				8	90				8	8				8	8				-90	8-				
	Les Night (db/)																											
	(App) (Opp)		53.62	98.51	58.311384			47.5	48.62	51.0501765			51.88	63.39	56.7105986			64.79	62.18	05.08.84.855			56.62	59.1	61.0449635			
	Receiver Base of Barier Ground Base of Barier Baraton (nt)		245	245				237	237				241	341				12	782				187	187				
	Sarra Gound Beallon (rs)		245	245				238	238				2.45	246				235	235				193	193				
	Bavation Change (e) Source Gound (m) Bevalen(rs)							1	1				9	9				22	22				9	9				
	Barter Roceiver Distance (rs.)							٠					٠	٠														
	Barrier Height (m)																											
١.	Barr 92		٠	٠				٠					٠	٠				٠	٠					٠				
	Barr 91		٠	٠				٠	٠				٠	٠										٠				
	Source Receiver		112	16				717	240				186	147				45	82				94	64				
	Receiver Height (r) (m)		1.2	1.2				1.2	1.2				1.2	1.2				17	1.2				1.2	1.2				
	Suface N Tune		-					-	1				-	-				-	-				1					
	8 Density																	•	٠					٠				_
	WOODS No Rows							٠	•				٠					•					•	٠				
																		•										_
	7060		1	1				3	3				3	3				0	3				3	3				4
	95	_	06	06				06	06				06	06				96	06				8	8				4
	91		-90	90-				90-80	9 -90				99-	99-				-90 8	90-				-90	90-				_
	SOURCE	Old Algrenner	8W memph well	Naw Algrimant EB	Това		Old Algrenant	Naw Algriment WB	New Algement EB	Total		решвуро	New Algrinant WB	New Algrand EB	Total		Old Algoment	New Algrand WB	83 nemtly wen	ROL		Old Alignment	New Algorism WB	New Algrand EB	KOT			
	RECENER	P338					ROS					R10					R11					R14						

Mitigation Calculations

Brian Butras	March 13, 2014
ENGINEER	DATE
602.H599	
PROJECT NUMBER	BASE DRAWING
	602.41.900

	Leq(Ngk) (dbA)																					
	LegDay or Leg Legytry (db)		47.17	47.65	50.426928	0		63.96	53.05	56.5390911	0		86.08	6411	57.6323251	0		55.45	61.29	56.880-4422	5.02210369	
	Base of Barriar Lea Beustlen (m) Leagt		188 4	188 4	207	Noise Reduction		187 6	187 6	565	Noise Reduction		189 5	189 5	979	Noise Reduction		216 5	216 5	56.8	Noise 5.02 Reduction	
	Receiver Ground Bases Beselfon (%) Bases		101	181		Reg		187	187		Red		188	188		Red		218 3	218 3		R S	
	Ground Gro		108	198 1				198 1	198 1				1 102	1 102				219 2	219 2			
	Elevation Change (e) Source Ground (m) Beration (n)			1 1				11 11					13 2	13 2				1 2	1 2			
	eve Change		3.00					198	198				147 1	147 1								
	Barter (m) Detarce (m)			370															8			
	Barrier 62 Height (m)		10	9				9	10				9	9				10	10			
١,	91 Barr 62		06	90				06	06				06	06				9	09			
			00-	00-				06-	8				6.	6.				8	-80			
	n Source n Receiver Dist (m)		441	409				193	238				182	217				4	26			
	Receiver Height (r) (m)		1.2	12				12	12				12	12				12	12			
	Surface 7 Type		-					-	-				-	-				-	-			
	s B Dansity		٠																٠			
	No. Rows		٠	٠					٠									٠	٠			
	woons			٠				٠														
	TOPO		4	+				4	4				4	4				4	4			
	95		8	06				06	8				06	06				06	06			
	10		8	00-				8	8				8	8				8	6			
	Les Night (db.h)																					
	Log (Cithy) (dBA)		41.17	47.65	50.426928			83.96	63.05	56.5390911			80.08	54.11	57.6323251			60.54	56.13	61.8825458		
	Base of Barier Bevilon (no																					
	Receiver Geomol Blavation (nt)		181	181				187	187				188	188				218	218			
	are Gound Bealion (n)		198	198				198	198				201	201				219	219			
	Bavation Change (ii) Surve Geund (m) Beuten (in)		-	2				11	11				13	13				-	1			
	Barter Rocelege Distance (rs)																					
	Barrier Height(m)																					
	Barr 62																					
	Source Receiver Dist(m)		441	409				193	226				182	217				44	82			
	Receiver Height (r) F (m)		1.2	1.2				1.2	1.2				1.2	1.2				1.2	1.2			
	Surface P. Type							-	-				-	-				-	-			
	® Density																					
	No. Rows 6																					
	WOOON N																					
	TOPO W		9	3				3	3				3	3				9	3			
	92 1		96	06				06	06				06	06				96	06			
	91		-90	-80				06-	-90				06-	06-				-80	-80			
F		ant.					nr.					314					ant.					
	SOURCE	Old Algriment	New Algement WB	New Algoment EB	Total		Old Algoment	New Algrand WB	New Algoment EB	Total		Old Mignment	New Algrant WB	New Algornant EB	Total		Old Algrment	New Algnment WB	New Algrand EB	Total		
	RECEIVER	R15					R16					R17					R18					